Fundamentals of Inviscid, Incompressible Flow

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Introduction

We will focus on fundamentals of inviscid, incompressible flow.

- # How low-speed tunnels work
- * Low-speed velocity measurement
- # Flow over streamlined bodies

Roadmap



Introduction



$V_{aircraft}~pprox~30mi/hr$

$V_{aircraft} \approx 300 mi/hr$



Courtesy of the U.S. Air Force.

Bernoulli's Equation

Solution Relates pressure and velocity in inviscid and incompressible flow.

$$\rho \left[\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + \frac{\partial u}{\partial z} \right] = -\frac{\partial p}{\partial x}$$

Euler's Equation: $dp = -\rho V dV$

$$p + \frac{1}{2}\rho V^2 = \text{constant}$$

Incompressible Flow in a Duct



 $\frac{\partial}{\partial t} \int_{V} + \int_{S} \rho V.dS = 0$

 $\frac{\partial}{\partial t} \int_{V} \rho d\nu + \int_{S} \rho V.dS = 0$

$$V_2 = \sqrt{\frac{2(p_1 - p_2)}{\rho[1 - (A_2/A_1)^2]}}$$

$$V_2 = \sqrt{\frac{2\rho g \Delta h}{\rho [1 - (A_2/A_1)^2]}}$$

Measurement of Airspeed

Solution With the second secon



Static Pressure

* Pressure is associated with rate of change of momentum of gas molecules impacting/crossing a surface.

* Pressure clearly related to the random motion of the molecules.

Static pressure is a measure of the purely random motion of molecules in a Lagrangian frame of reference

When flow moves over point A, the pressure felt is due only to the random motion of the particles - Static pressure.

The Pitot-Static Probe



The Pitot-Static Probe



The probe should be long, streamlined such that the static pressure over a substantial portion of the probe is equal to free stream static pressure



Pitot-Static Probe Design



Pitot-static probes should be located in a position away from influences of local flow field. Son aircraft, static pressure is generally obtained by a properly placed static pressure tap on the fuselage.

Pressure Coefficient

Solution Pressure coefficient C_p - *a similarity parameter* used through out aerodynamics, from incompressible to hypersonic flow.

$$C_{p} = \frac{p - p_{\infty}}{q_{\infty}} \qquad q_{\infty} = \frac{1}{2}\rho_{\infty}V_{\infty}^{2}$$

For incompressible flow, $C_{p} = 1 - \left(\frac{V}{V_{\infty}}\right)^{2}$

- For incompressible flow, *pressure coefficient at stagnation point is always 1.0* (can be greater than 1.0 for compressible flow).
 In regions of flow where local velocity is less than freestream velocity, pressure coefficient will be negative (local pressure is
 - less than freestream pressure).

Solution From the worked out example C_p is obviously unchanged as the velocity is increased.

- ***** From dimensional analysis, C_p depends on Mach number, Reynolds number, shape, orientation of body and location on body.
- ** In this example, M and Re and not in picture (why?). C_p only depends on location, shape and orientation of the body.
- **Hence,* C_p *will not change with free stream velocity or density as long as the flow is incompressible and inviscid.*

Solution For such flows, if C_p distribution can be determined by some means beforehand, it will remain the same for all freestream values of velocity and density.

So The velocity when $C_p = -5.3$ was calculated to be 753ft/s. Is this correct?

$$M = \frac{753}{1117} \approx 0.7$$

- Solution Here, the flow has expanded locally into the compressible flow regime.
- Solution C_p is incorrect. Set C_p is incorrect.

Solution Even if the model is being tested in a low-speed wind tunnel, the flow can some times accelerate to achieve high Mach numbers that it must be considered compressible.

Governing Equations

Incompressible flow: $\nabla V = 0$

 $V = \nabla \Phi$

- $\Rightarrow \nabla \cdot (\nabla \Phi) = 0$
- $\Rightarrow \nabla^2 \Phi = 0 \text{ and } \nabla^2 \psi = 0$

Solution is the Laplace equation, the solutions of which are called the harmonic functions.

Solutions of the Incompressible flows can be described by the solutions of the Laplace equation.

Solution From Incompressible flows are governed by Laplace equation which is linear.

Solution Linearity implies, a complicated flow pattern can be constructed by adding together various elementary flows which also are linear.

Different elementary flows
 ** Uniform flow
 ** Source/Sink flow
 ** Doublet
 ** Vortex flow
 ** Combination of the above

The Kutta-Joukowski Theorem



$$\Gamma = \oint_A V.ds$$

 $L' = \rho_{\infty} \overline{V_{\infty}} \Gamma$

The Kutta-Joukowski Theorem

Lifting flow over a cylinder = uniform flow + doublet + vortex
 ** All three are irrotational except for vortex
 ** Vortex has infinite vorticity at the origin
 ** So, lifting flow over the cylinder is irrotational at every point except origin.

$$\Gamma = \oint V.ds = 0$$

not including origin

Similar arguments for flow over airfoil

*Flow outside the airfoil is irrotational

*Circulation by not including the airfoil is zero

*****Kutta-Joukowski theorem requires inclusion of airfoil body to obtain finite circulation (*sum of all vortex's strengths that constitue the airfoil*)

Real Flow over a Circular Cylinder

