

①

Our Combustion model

$$\rho \left(\frac{\partial Y_F}{\partial t} + (u \cdot \nabla) Y_F \right) - \nabla \cdot (\rho D \nabla Y_F) = -k_p^2 Y_F Y_O$$

$$\rho \left(\frac{\partial Y_O}{\partial t} + (u \cdot \nabla) Y_O \right) - \nabla \cdot (\rho D \nabla Y_O) = -r k_p^2 Y_F Y_O$$

$$\rho \left(\frac{\partial T}{\partial t} + (u \cdot \nabla) T \right) - \nabla \cdot (\rho c_p \nabla T) = + k_p^2 Y_F Y_O \frac{q}{c_p}$$

$$k(T) = A T^\alpha \exp\left(\frac{T_a}{T}\right) \quad \text{u-fluid model drives combustion.}$$

Define z such that

$$\rho \left(\frac{\partial z}{\partial t} + (u \cdot \nabla) z \right) - \nabla \cdot (\rho D \nabla z) = 0$$

The solution is caught in a center manifold such that
 $Y_F = Y_F(z, T)$ and $Y_O = Y_O(z, T)$

Center manifold expansion

Expand to 1st order:

$$Y_F = A_1 + A_2 z + A_3 T$$

$$Y_O = B_1 + B_2 z + B_3 T$$

To give some meaning to z we demand that:

$$\begin{cases} Y_F(1, T_F, \varnothing) = 1 \\ Y_O(1, T_F, \varnothing) = 0 \\ Y_F(0, T_O, \varnothing) = 0 \\ Y_O(0, T_O, \varnothing) = 1 \end{cases} \Leftrightarrow \begin{cases} A_1 + A_2 + A_3 T_F = 1 & (1) \\ B_1 + B_2 + B_3 T_F = 0 & (2) \\ A_1 + A_3 T_O = 0 & (3) \\ B_1 + B_3 T_O = 0 & (4) \end{cases}$$

$$A_1 = -A_3 T_O \Rightarrow -A_3 T_O + A_2 + A_3 T_F = 1 \Rightarrow A_2 = 1 + A_3 (T_O - T_F)$$

$$B_1 = -B_3 T_O \Rightarrow -B_3 T_O + B_2 + B_3 T_F = 0 \Rightarrow B_2 = A_3$$

→ interpretation.

(2)

$$\begin{cases} Y_F(1, T_F, \phi) = Y_{F, \phi} \\ Y_0(1, T_F, \phi) = 0 \\ Y_F(0, T_0, \phi) = 0 \\ Y_0(0, T_0) = Y_{0, \phi} \end{cases} \Leftrightarrow \begin{cases} A_1 + A_2 + A_3 T_F = Y_{F, \phi} \\ B_1 + B_2 + B_3 T_{0F} = 0 \\ A_1 + A_3 T_0 = 0 \\ B_1 + B_3 T_0 = Y_{0, \phi} \end{cases}$$

Write A_1, A_2 in terms of A_3 .

$$A_1 = -A_3 T_0.$$

$$A_2 = Y_{F, \phi} - A_1 - A_3 T_F = Y_{F, \phi} + A_3 T_0 - A_3 T_F = Y_{F, \phi} + A_3 (T_0 - T_F).$$

Write B_1, B_2 in terms of B_3 :

$$B_1 = Y_{0, \phi} - B_3 T_0.$$

$$B_2 = -B_1 - B_3 T_F = -(Y_{0, \phi} - B_3 T_0) - B_3 T_F = -Y_{0, \phi} + B_3 (T_0 - T_F).$$

We obtain:

$$Y_F = -A_3 T_0 + (Y_{F, \phi} + A_3 (T_0 - T_F)) Z + A_3 T$$

$$Y_0 = (Y_{0, \phi} - B_3 T_0) + (-Y_{0, \phi} + B_3 (T_0 - T_F)) Z + B_3 T.$$

To obtain A_3 and B_3 :

$$\text{Define } \mathcal{L} \xi = \rho \left(\frac{\partial \xi}{\partial t} + (u \cdot \nabla) \xi \right) - \nabla \cdot (\rho D \nabla \xi)$$

Then we know that

$$\mathcal{L} Y_F = -k \rho^2 Y_F Y_0.$$

$$\mathcal{L} Y_0 = -r k \rho^2 Y_F Y_0.$$

$$\mathcal{L} T = +k \rho^2 Y_F Y_0 \frac{q}{\rho c_p} \quad \mathcal{L} Z = 0$$

Write:

$$\begin{aligned} \mathcal{L} Y_F &= \mathcal{L} (-A_3 T_0 + (Y_{F, \phi} + A_3 (T_0 - T_F)) Z + A_3 T) = \\ &= (Y_{F, \phi} + A_3 (T_0 - T_F)) \mathcal{L} Z + A_3 \mathcal{L} T = \\ &= A_3 \mathcal{L} T = +k \rho^2 Y_F Y_0 \frac{q}{c_p} A_3 \end{aligned}$$

$$\text{then: } \frac{q}{c_p} A_3 = 1 - 1 \Rightarrow A_3 = -\frac{c_p}{q}.$$

$$\text{Also } \mathcal{L} Y_0 = k \rho^2 Y_F Y_0 \frac{q}{c_p} B_3 = -r k \rho^2 Y_F Y_0 \Rightarrow B_3 = -\frac{r c_p}{q}.$$

Define $\tau = c_p / q$. $\tau_0 = q / c_p$.

Then our equations become:

③

Define non-dimensionalized temperature:

$$\tau = \frac{C_p T}{q}, \quad \tau_F = \frac{C_p T_F}{q}, \quad \tau_0 = \frac{C_p T_0}{q}$$

Our equations become:

$$Y_F = \tau_0 + (Y_{F,0} - (\tau_0 - \tau_F)) z - \tau$$

$$Y_0 = (Y_{0,0} + r\tau_0) - (Y_{0,0} + r(\tau_0 - \tau_F)) z - r\tau$$

Another remarkable property of this manifold is that z can be written as an affine function of Y_F and Y_0 : $z = \lambda_1 Y_F + \lambda_2 Y_0 + \lambda_3$.

Abbreviate: $Y_F = A_1 + A_2 z - \tau$

$$Y_0 = B_1 + B_2 z - r\tau$$

Then: $z = \lambda_1 (A_1 + A_2 z - \tau) + \lambda_2 (B_1 + B_2 z - r\tau) + \lambda_3 =$

$$= (A_1 \lambda_1 + B_1 \lambda_2 + \lambda_3) + (A_2 \lambda_1 + B_2 \lambda_2) z - (\lambda_1 + r \lambda_2) \tau$$

It follows that

$$\begin{cases} A_1 \lambda_1 + B_1 \lambda_2 + \lambda_3 = 0 \\ A_2 \lambda_1 + B_2 \lambda_2 = 1 \\ \lambda_1 + r \lambda_2 = 0 \end{cases} \Leftrightarrow \begin{bmatrix} A_1 & B_1 & 1 \\ A_2 & B_2 & 0 \\ 1 & r & 0 \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

$$\Leftrightarrow \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \end{bmatrix} = \frac{1}{rA_2 - B_2} \begin{bmatrix} 0 & r & -B_2 \\ 0 & -1 & A_2 \\ (rA_2 - B_2) & -(rA_1 - B_1) & - \end{bmatrix}$$

$$\begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \lambda_3 \end{bmatrix}$$

The solution is:

$$\lambda_1 = \frac{r}{rA_2 - B_2}, \quad \lambda_2 = \frac{-1}{rA_2 - B_2}, \quad \lambda_3 = \frac{B_1 - rA_1}{rA_2 - B_2}$$

Therefore:

$$z = \lambda_1 Y_F + \lambda_2 Y_0 + \lambda_3 = \frac{r Y_F - Y_0 + (B_1 - rA_1)}{rA_2 - B_2} = \frac{r Y_F - Y_0 - (rA_1 - B_1)}{rA_2 - B_2}$$

Substitute

$$rA_1 - B_1 = r(\tau_0) - (Y_{0,0} + r\tau_0) = r(\tau_0 - \tau) - Y_{0,0}$$

$$rA_2 - B_2 = r(Y_{F,0} + r\tau) - (Y_{0,0} + r(\tau_0 - \tau_F)) = (r+1)Y_{0,0} + r$$

$$rA_2 - B_2 = r(Y_{F,0} - (\tau_0 - \tau_F)) + (Y_{0,0} + r(\tau_0 - \tau_F)) \quad \text{wow!}$$

$$= (r+1)Y_{0,0} + r$$

and we find that:

(2)

$$z = \frac{rY_F - Y_0 + Y_{0,\phi} + r(Y_F - Y_{0,\phi})}{rY_{F,\phi} - Y_{0,\phi}}$$

Note that there is no dependence on τ , τ_F or τ_0 !!

To summarize:

The center-manifold approximation to our model is:

$$\rho \left(\frac{\partial z}{\partial t} + (u \cdot \nabla) z \right) - \nabla \cdot (\rho D \nabla z) = 0.$$

$$\rho \left(\frac{\partial \tau}{\partial t} + (u \cdot \nabla) \tau \right) - \nabla \cdot (\rho D \nabla \tau) = k\rho^2 Y_F Y_0.$$

$$Y_F = \tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z - \tau = Y_F(z, \tau).$$

$$Y_0 = (Y_{0,\phi} + r\tau_0) - (Y_{0,\phi} + r(\tau_0 - \tau_F)) z - r\tau$$

~~$$k = A T^a \exp(T_0/T) = A c^a$$~~

and
$$z = \frac{rY_F - Y_0 + Y_{0,\phi}}{rY_{F,\phi} - Y_{0,\phi}}$$

If we take this as a definition of z , then the equations relating Y_F, Y_0 with z, τ can be used to obtain τ up to 1st order.

Recall $\tau = \frac{C\rho T}{q}$, $\tau_F = \frac{C\rho T_F}{q}$, $\tau_0 = \frac{C\rho T_0}{q}$.

(5)

Fast chemistry limitAssumption : $Y_F Y_O = 0$.

(F and O can not coexist bc they react immediately)

Consider also $\frac{r Y_F - Y_O + Y_{O, \infty}}{r Y_{F, \infty} + Y_{O, \infty}} = Z$.

$$\text{or } r Y_F - Y_O + Y_{O, \infty} = Z (r Y_{F, \infty} + Y_{O, \infty})$$

To solve, two cases:

Case 1 : $Y_F \neq 0$.Then $Y_O = 0 \Leftrightarrow$

$$r Y_F + Y_{O, \infty} - Z (r Y_{F, \infty} + Y_{O, \infty}) = 0 \Leftrightarrow$$

$$r Y_F = Z (r Y_{F, \infty} + Y_{O, \infty}) - Y_{O, \infty}$$

$$\text{Requires : } r Y_F > 0 \Leftrightarrow Z > \frac{Y_{O, \infty}}{r Y_{F, \infty} + Y_{O, \infty}}$$

$$\text{Define : } z_{st} = \frac{Y_{O, \infty}}{r Y_{F, \infty} + Y_{O, \infty}}$$

$$\text{Then : } r Y_F = (r Y_{F, \infty} + Y_{O, \infty}) (Z - z_{st}) H(Z - z_{st}) \text{ for all } 0 \leq Z \leq 1$$

Also Moreover

$$1 - z_{st} = \frac{r Y_{F, \infty} + Y_{O, \infty} - Y_{O, \infty}}{r Y_{F, \infty} + Y_{O, \infty}} = \frac{r Y_{F, \infty}}{r Y_{F, \infty} + Y_{O, \infty}} \Rightarrow$$

$$\Rightarrow r Y_{F, \infty} + Y_{O, \infty} = \frac{r Y_{F, \infty}}{1 - z_{st}}$$

$$\text{Then : } r Y_F = r Y_{F, \infty} \frac{Z - z_{st}}{1 - z_{st}} H(Z - z_{st}) \Rightarrow$$

$$\Rightarrow \boxed{Y_F = Y_{F, \infty} \frac{Z - z_{st}}{1 - z_{st}} H(Z - z_{st})}$$

Case 2 : $Y_O \neq 0$ Then $Y_F = 0 \Leftrightarrow$

$$Y_O - Y_{O, \infty} + Z (r Y_{F, \infty} + Y_{O, \infty}) = 0 \Leftrightarrow$$

$$Y_O = Y_{O, \infty} - Z (r Y_{F, \infty} + Y_{O, \infty}) =$$

$$= (r Y_{F, \infty} + Y_{O, \infty}) (z_{st} - Z) =$$

$$= Y_{O, \infty} \frac{z_{st} - Z}{z_{st}}$$

 $Y_O > 0 \Rightarrow$ require $Z < z_{st}$, therefore

⑥

$$Y_0 = Y_{0,\phi} \frac{z_{st} - z}{z_{st}} H(z_{st} - z).$$

Now we can relate the temperature τ as a function of z :

Use: $Y_F = Y_F(z, \tau) = \tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z - \tau \Rightarrow$

$$\begin{aligned} \Rightarrow \tau &= \tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z - Y_F = \\ &= \tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z - Y_{F,\phi} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st}). \end{aligned}$$

► For $z < z_{st}$: $\tau = \tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z.$

Use: $Y_0 = Y_0(z, \tau) = (Y_{0,\phi} + r\tau_0) - (Y_{0,\phi} + r(\tau_0 - \tau_F)) z - r\tau \Rightarrow$

$$\Rightarrow r\tau = (Y_{0,\phi} + r\tau_0) - (Y_{0,\phi} + r(\tau_0 - \tau_F)) z - Y_0$$

► For $z > z_{st}$: $r\tau = (Y_{0,\phi} + r\tau_0) - (Y_{0,\phi} + r(\tau_0 - \tau_F)) z$

In general:

$$\tau = \left[\tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z \right] H(z - z_{st}) + \left[(Y_{0,\phi} + r\tau_0) - (Y_{0,\phi} + r(\tau_0 - \tau_F)) z \right] \frac{H(z_{st} - z)}{r} =$$

Putting this all-together, in the fast chemistry limit, z is the leading equation and Y_F, Y_0 and τ are slaves to z .

$$\tau = \left[\tau_0 + (Y_{F,\phi} - (\tau_0 - \tau_F)) z \right] H(z - z_{st}) + \left[(Y_{0,\phi} + r\tau_0) - (Y_{0,\phi} + r(\tau_0 - \tau_F)) z \right] \frac{H(z_{st} - z)}{r}.$$

(7)

Averaging w_F on the fast chemistry limitNote that $w_0 = r w_F$. Want w_F .

$$\begin{aligned} w_F &= \rho \left(\frac{\partial Y_F}{\partial t} + (u \cdot \nabla) Y_F \right) - \nabla \cdot (\rho D \nabla Y_F) = \\ &= \rho \left(\frac{\partial Y_F}{\partial t} + (u \cdot \nabla) Y_F \right) - D \nabla \cdot (\rho \nabla Y_F) \end{aligned}$$

where $Y_F = Y_{F,0} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st})$.

Define $L(A) = \rho \left(\frac{\partial A}{\partial t} + (u \cdot \nabla) A \right) - D \nabla \cdot (\rho \nabla A)$.

Then $w_F = L \left(Y_{F,0} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st}) \right)$.

To compute this, note that L is linear operator, therefore:

$$L(A+B) = L(A) + L(B)$$

$$L(\lambda A) = \lambda L(A), \text{ for } \lambda = \text{const.}$$

Want to find $L(AB)$ and $L'(A(B))$.Decompose: $L = L_1 - D \nabla \cdot (\rho \nabla)$. L_1 respects the product rule and the chain rule:

$$L_1(AB) = A L_1(B) + B L_1(A)$$

$$L_1(A(B)) = \frac{\partial A}{\partial B} L_1(B)$$

Now consider:

$$\begin{aligned} \nabla \cdot (\rho \nabla (AB)) &= \nabla \cdot (\rho A \nabla B + \rho B \nabla A) = \nabla \cdot (\rho A \nabla B) + \nabla \cdot (\rho B \nabla A) = \\ &= \rho A \nabla^2 B + \nabla(\rho A) \cdot \nabla B + \rho B \nabla^2 A + \nabla(\rho B) \cdot \nabla A = \\ &= \rho A \nabla^2 B + \rho B \nabla^2 A + (\rho \nabla A + A \nabla \rho) \cdot \nabla B + (\rho \nabla B + B \nabla \rho) \cdot \nabla A \\ &= A \nabla \cdot (\rho \nabla B) + B \nabla \cdot (\rho \nabla A) + \rho \nabla B \cdot \nabla A + \rho \nabla A \cdot \nabla B = \\ &= A \nabla \cdot (\rho \nabla B) + B \nabla \cdot (\rho \nabla A) + 2\rho \nabla A \cdot \nabla B. \end{aligned}$$

It follows that

$$\begin{aligned} L(AB) &= L_1(AB) - D \nabla \cdot (\rho \nabla (AB)) = \\ &= A L_1(B) + B L_1(A) - D (A \nabla \cdot (\rho \nabla B) + B \nabla \cdot (\rho \nabla A) + 2\rho \nabla A \cdot \nabla B) = \\ &= A (L_1(B) - D \nabla \cdot (\rho \nabla B)) + B (L_1(A) - D \nabla \cdot (\rho \nabla A)) - 2\rho D \nabla A \cdot \nabla B = \\ &= A L(B) + B L(A) - 2\rho D \nabla A \cdot \nabla B. \end{aligned}$$

8)

Also

$$\nabla \cdot (\rho \nabla A(B)) = \nabla \cdot \left(\rho \frac{\partial A}{\partial B} \nabla B \right) = \frac{\partial A}{\partial B} \nabla \cdot (\rho \nabla B) + \rho \nabla B \cdot \nabla \left(\frac{\partial A}{\partial B} \right)$$

therefore

$$\begin{aligned} L(A(B)) &= L_L(A(B)) - \rho D \nabla \cdot (\rho \nabla A(B)) = \\ &= \frac{\partial A}{\partial B} L_L(B) - \rho D \left(\frac{\partial A}{\partial B} \nabla \cdot (\rho \nabla B) + \rho \nabla B \cdot \nabla \left(\frac{\partial A}{\partial B} \right) \right) = \\ &= \frac{\partial A}{\partial B} \left(L_L(B) - \rho D \nabla \cdot (\rho \nabla B) \right) - \rho D \nabla \left(\frac{\partial A}{\partial B} \right) \cdot \nabla B \\ &= \frac{\partial A}{\partial B} L(B) - \rho D \nabla \left(\frac{\partial A}{\partial B} \right) \cdot \nabla B. \end{aligned}$$

We have then:

$$\begin{aligned} L(AB) &= AL(B) + BL(A) - 2\rho D (\nabla A \cdot \nabla B) \\ L(A(B)) &= \frac{\partial A}{\partial B} L(B) - \rho D \nabla \left(\frac{\partial A}{\partial B} \right) \cdot \nabla B \end{aligned}$$

Now we can compute \dot{w}_F :

$$\begin{aligned} \dot{w}_F &= L \left(Y_{F, \rho} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st}) \right) = Y_{F, \rho} L \left(\frac{z - z_{st}}{1 - z_{st}} H(z - z_{st}) \right) = \\ &= Y_{F, \rho} L \left(\frac{z - z_{st}}{1 - z_{st}} \right) H(z - z_{st}) + Y_{F, \rho} \frac{z - z_{st}}{1 - z_{st}} L(H(z - z_{st})) - 2\rho D \left[\nabla \left(\frac{z - z_{st}}{1 - z_{st}} \right) \cdot \nabla (H(z - z_{st})) \right] Y_{F, \rho} \end{aligned}$$

Take the terms individually:

1st term:

$$L \left(\frac{z - z_{st}}{1 - z_{st}} \right) = \frac{1}{1 - z_{st}} L(z) = 0.$$

2nd term

$$\begin{aligned} L(H(z - z_{st})) &= \delta(z - z_{st}) L(z - z_{st}) - \rho D \nabla (\delta(z - z_{st})) \cdot \nabla (z - z_{st}) = \\ &= \delta(z - z_{st}) L(z) - \rho D \delta'(z - z_{st}) \nabla z \cdot \nabla z = \\ &= -\rho D N \delta'(z - z_{st}) \end{aligned}$$

where we defined

$$N = D (\nabla z \cdot \nabla z) \leftarrow \text{scalar dissipation}$$

3rd term:

$$\nabla \left(\frac{z - z_{st}}{1 - z_{st}} \right) \cdot \nabla (H(z - z_{st})) = \frac{1}{1 - z_{st}} \nabla z \cdot \left[\delta(z - z_{st}) \nabla z \right] = \frac{\delta(z - z_{st}) (\nabla z \cdot \nabla z)}{1 - z_{st}}$$

(9)

Putting it all together:

$$\begin{aligned}
 \dot{w}_F &= Y_{F,i} \rho \frac{z-z_{st}}{1-z_{st}} \left[-\rho N \delta'(z-z_{st}) \right] + 2\rho D \frac{\delta(z-z_{st})}{1-z_{st}} (\nabla z \cdot \nabla z) \cdot Y_{F,i} \rho = \\
 &= \frac{Y_{F,i} \rho N}{1-z_{st}} \left[-(z-z_{st}) \delta'(z-z_{st}) + 2\delta(z-z_{st}) \right] = \\
 &= Y_{F,i} \rho N \frac{1}{1-z_{st}} \left[-\delta(z-z_{st}) + 2\delta(z-z_{st}) \right] = \\
 &= \rho N Y_{F,i} \frac{\delta(z-z_{st})}{1-z_{st}}.
 \end{aligned}$$

therefore we obtained:

$$\dot{w}_F = \rho N Y_{F,i} \frac{\delta(z-z_{st})}{1-z_{st}}$$

Remark: reaction takes place at regions where $z = z_{st}$.
 this is then the physical meaning of z_{st} .

Hydrogen/air = 0.028.

Methane/air = 0.05

DNS = 0.5 !

↳ experimentalists also increase z_{st} in their experiments
 in order to see more detail.

We do this only for calculation purposes.

Remark: If we assume that $\rho = \text{const}$ (ex. open jet).
 then $\rho = \frac{\rho R T}{w}$, $w = \left(\sum \frac{Y_i}{w_i} \right)^{-1} = w(z)$

$T = T(z)$.

$\rho = \rho^{eq}(z)$ density is also a function of z .
 we may then write:

$$\begin{aligned}
 \langle \dot{w}_F \rangle &= \int_0^{+\infty} \int_0^1 \rho(z) N Y_{F,i} \frac{\delta(z-z_{st})}{1-z_{st}} P(z, N; x) dz dN = \\
 &= \int_0^{+\infty} \rho(z_{st}) N Y_{F,i} \frac{P(z_{st}, N; x)}{1-z_{st}} dN.
 \end{aligned}$$

①

Frozen chemistry limit

No interaction between chemistry and mixing. Mixing takes place first. Chemistry follows.

$$T = \tau_0 : Y_F = Y_{F,0} z$$

$$Y_O = Y_{O,0} (1 - z)$$

The time it takes for mixing to complete is:

$$T_{mix} \sim \frac{l}{u} \quad (\text{due to turbulence})$$

The time it takes for the chemistry:

$$T_{ch} \sim \frac{1}{k_p}$$

$$\text{Damköhler number: } Da = \frac{T_{mix}}{T_{ch}}$$

Frozen chemistry limit: $Da \ll 1$.

Fast chemistry limit

F + O cannot mix. They immediately react into product. Therefore $Y_F Y_O = 0$.

$$\text{Also: } \frac{r Y_F - Y_O + Y_{O,0}}{r Y_{F,0} + Y_{O,0}} = z$$

Solve for Y_F, Y_O the following perturbed equations:

$$Y_F Y_O = \epsilon$$

$$r Y_F - Y_O + Y_{O,0} = z (r Y_{F,0} + Y_{O,0})$$

$$\text{Write } Y_O = r Y_F + Y_{O,0} - z (r Y_{F,0} + Y_{O,0})$$

$$Y_F Y_O = 0 \Leftrightarrow$$

$$Y_F (r Y_F + Y_{O,0} - z (r Y_{F,0} + Y_{O,0})) = 0$$

If $Y_F \neq 0$,

$$r Y_F + Y_{O,0} - z (r Y_{F,0} + Y_{O,0}) = 0$$

$$Y_F = \frac{z (r Y_{F,0} + Y_{O,0}) - Y_{O,0}}{r}$$

$$\text{requires: } z \gg \frac{Y_{O,0}}{r Y_{F,0} + Y_{O,0}}$$

(2)

Write $rY_F = Y_0 - Y_{0,\phi} + z (rY_{F,\phi} + Y_{0,\phi})$ $Y_0 > 0.$

$Y_0 rY_F = 0 \Leftrightarrow$

$Y_0 - Y_{0,\phi} + z (rY_{F,\phi} + Y_{0,\phi}) = 0. \Leftrightarrow$

$Y_0 = Y_{0,\phi} - z (rY_{F,\phi} + Y_{0,\phi}). > 0.$

But $z \ll \frac{Y_{0,\phi}}{rY_{F,\phi} + Y_{0,\phi}}$

Define: $z_{st} = \frac{Y_{0,\phi}}{rY_{F,\phi} + Y_{0,\phi}}$, $H(z) = \begin{cases} 1, & z > 0 \\ 0, & z < 0 \end{cases}$
Heaviside function.

Then we obtained:

$rY_F = [z (rY_{F,\phi} + Y_{0,\phi}) - Y_{0,\phi}] H(z - z_{st})$

$= \frac{z_{st}}{1 - z_{st}} (rY_{F,\phi} + Y_{0,\phi}) (z - z_{st}) H(z - z_{st}) =$
 $= \frac{Y_{0,\phi} (z - z_{st})}{1 - z_{st}} H(z - z_{st}).$

$1 - z_{st} = \frac{rY_{F,\phi} + Y_{0,\phi} - Y_{0,\phi}}{rY_{F,\phi} + Y_{0,\phi}} = \frac{rY_{F,\phi}}{rY_{F,\phi} + Y_{0,\phi}} \Rightarrow rY_{F,\phi} + Y_{0,\phi} = \frac{rY_{F,\phi}}{1 - z_{st}}$

then

$Y_F = Y_{F,\phi} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st})$

$Y_0 = Y_{0,\phi} - z (rY_{F,\phi} + Y_{0,\phi}) = (rY_{F,\phi} + Y_{0,\phi}) (z_{st} - z) =$
 $= \frac{Y_{0,\phi} (z - z_{st})}{z_{st}} H(z_{st} - z).$

so $Y_0 = Y_{0,\phi} \frac{z - z_{st}}{z_{st}} H(z_{st} - z)$

What about the temperature?

(3)

Take

$$\frac{C_p}{q} (T - T_0) = Y_{F,0} z - Y_F = Y_{F,0} z - Y_{F,0} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st}) =$$

$$= Y_{F,0} \left(z - \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st}) \right)$$

~~$$\frac{C_p}{q} (T - T_0) = Y_{O,0} (1 - z) - Y_{O,0} \frac{z - z_{st}}{z_{st}} H(z - z_{st})$$~~

For $z < z_{st}$ we obtain:

$$\frac{C_p}{q} (T - T_0) = Y_{F,0} z$$

For $z > z_{st}$

$$\frac{C_p}{q} (T - T_0) = Y_{O,0} (1 - z) - Y_0 = Y_{O,0} (1 - z)$$

Putting these together we get.

$$\frac{C_p}{q} (T - T_0) = Y_{F,0} z H(z_{st} - z) + Y_{O,0} (1 - z) H(z - z_{st}) =$$

$$= Y_{F,0} z (1 - H(z_{st} - z)) + Y_{O,0} (1 - z) H(z - z_{st}) =$$

$$= Y_{F,0} z + [Y_{O,0} (1 - z) - Y_{F,0} z] H(z - z_{st})$$

Thus:

$$T = T_0 + \frac{q Y_{F,0}}{C_p} z + \frac{q}{C_p} [Y_{O,0} (1 - z) - Y_{F,0} z] H(z - z_{st})$$

Putting this all-together, in the fast-chemistry limit:

$$\frac{\partial z}{\partial t} + (u \cdot \nabla) z - \nabla \cdot (\rho D \nabla z) = 0$$

$$Y_F = Y_{F,0} \frac{z - z_{st}}{1 - z_{st}} H(z - z_{st})$$

$$Y_O = Y_{O,0} \frac{z - z_{st}}{z_{st}} H(z_{st} - z)$$

$$T = T_0 + \frac{q}{C_p} \left\{ Y_{F,0} z + [Y_{O,0} (1 - z) - Y_{F,0} z] H(z - z_{st}) \right\}$$

$$\text{where: } z_{st} = \frac{Y_{O,0}}{n Y_{F,0} + Y_{O,0}}$$