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▼ Conditional moment closure model

The full equations that govern $F+O \rightarrow P$ are

$$\frac{\partial Y_F}{\partial t} = D \nabla^2 Y_F - (u \cdot \nabla) Y_F - A Y_F Y_O$$

$$\frac{\partial Y_O}{\partial t} = D \nabla^2 Y_O - (u \cdot \nabla) Y_O - r A Y_F Y_O$$

If we evolve a z -scalar by

$$\frac{\partial z}{\partial t} = D \nabla^2 z - (u \cdot \nabla) z$$

and initialize z appropriately then $z = \frac{r Y_F - Y_O + Y_{O,\sigma}}{r Y_{F,\sigma} + Y_{O,\sigma}}$

If we assume that $Y_{O,\sigma} = Y_{F,\sigma} = 1$ then:

$$z = \frac{r Y_F - Y_O + 1}{r + 1}$$

Now define $Q_F(n, t) = \langle Y_F | z = n \rangle_t$

$$Q_O(n, t) = \langle Y_O | z = n \rangle_t$$

→ conditional averages of Y_F, Y_O for $z = n$ at time t .

The actual values $Y_F(\vec{x}, t)$ are distributed around $Q_F(z(\vec{x}, t), t)$ with a "small" deviation. We write then:

$$Y_F(\vec{x}, t) = Q_F(z(\vec{x}, t), t) + y_F(\vec{x}, t)$$

$$Y_O(\vec{x}, t) = Q_O(z(\vec{x}, t), t) + y_O(\vec{x}, t)$$

The CMC model wants to describe the behaviour of Q_F and Q_O . To do that we substitute these equations to the full PDEs for Y_F and Y_O .

$$\frac{\partial Y_F}{\partial t} = \frac{\partial y_F}{\partial t} + \frac{\partial Q_F}{\partial z} \frac{\partial z}{\partial t} + \frac{\partial Q_F}{\partial t}$$

$$\frac{\partial Y_O}{\partial t} = \frac{\partial y_O}{\partial t} + \frac{\partial Q_O}{\partial z} \frac{\partial z}{\partial t} + \frac{\partial Q_O}{\partial t}$$

Also, for x, y, z derivatives:

$$\frac{\partial Y_F}{\partial x} = \frac{\partial y_F}{\partial x} + \frac{\partial Q_F}{\partial z} \frac{\partial z}{\partial x}$$

$$\frac{\partial Y_F}{\partial y} = \frac{\partial y_F}{\partial y} + \frac{\partial Q_F}{\partial z} \frac{\partial z}{\partial y}$$

$$\frac{\partial Y_F}{\partial z} = \frac{\partial y_F}{\partial z} + \frac{\partial Q_F}{\partial z} \frac{\partial z}{\partial z}$$

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In vector notation:

$$\nabla Y_F = \nabla y_F + \frac{\partial Q_F}{\partial z} \nabla z \quad \text{and} \quad \nabla Y_0 = \nabla y_0 + \frac{\partial Q_0}{\partial z} \nabla z.$$

For second derivatives:

$$\begin{aligned} \frac{\partial^2 Y_F}{\partial x^2} &= \frac{\partial^2 y_F}{\partial x^2} + \frac{\partial}{\partial x} \left(\frac{\partial Q_F}{\partial z} \frac{\partial z}{\partial x} \right) = \\ &= \frac{\partial^2 y_F}{\partial x^2} + \frac{\partial^2 z}{\partial x^2} \frac{\partial Q_F}{\partial z} + \frac{\partial z}{\partial x} \frac{\partial}{\partial x} \left(\frac{\partial Q_F}{\partial z} \right) = \\ &= \frac{\partial^2 y_F}{\partial x^2} + \frac{\partial^2 z}{\partial x^2} \frac{\partial Q_F}{\partial z} + \left(\frac{\partial z}{\partial x} \right)^2 \frac{\partial^2 Q_F}{\partial z^2} \end{aligned}$$

and likewise for the y, z derivatives. Then:

$$\nabla^2 Y_F = \nabla^2 y_F + \frac{\partial Q_F}{\partial z} \nabla^2 z + (\nabla z \cdot \nabla z) \frac{\partial^2 Q_F}{\partial z^2}.$$

$$\nabla^2 Y_0 = \nabla^2 y_0 + \frac{\partial Q_0}{\partial z} \nabla^2 z + (\nabla z \cdot \nabla z) \frac{\partial^2 Q_0}{\partial z^2}.$$

To obtain the CMC equations compare

$$\frac{\partial Y_F}{\partial t} = \frac{\partial y_F}{\partial t} + \frac{\partial Q_F}{\partial z} \frac{\partial z}{\partial t} + \frac{\partial Q_F}{\partial t}$$

$$\frac{\partial Y_F}{\partial t} = D \nabla^2 Y_F - (u \cdot \nabla) Y_F - A Y_F Y_0$$

using the substitutions:

$$\frac{\partial z}{\partial t} = D \nabla^2 z - (u \cdot \nabla) z$$

$$\nabla^2 Y_F = \nabla^2 y_F + \frac{\partial Q_F}{\partial z} \nabla^2 z + \frac{\partial^2 Q_F}{\partial z^2} (\nabla z \cdot \nabla z).$$

$$(u \cdot \nabla) Y_F = \frac{\partial Q_F}{\partial z} (u \cdot \nabla) z + (u \cdot \nabla) y_F.$$

If we do that we obtain:

$$\begin{aligned} \frac{\partial y_F}{\partial t} + \frac{\partial Q_F}{\partial z} (D \nabla^2 z - (u \cdot \nabla) z) + \frac{\partial Q_F}{\partial t} &= D \left[\nabla^2 y_F + \frac{\partial Q_F}{\partial z} \nabla^2 z + \frac{\partial^2 Q_F}{\partial z^2} (\nabla z \cdot \nabla z) \right] \\ &\quad - \left[\frac{\partial Q_F}{\partial z} (u \cdot \nabla) z + (u \cdot \nabla) y_F \right] - A (Q_F + y_F) (Q_0 + y_0). \end{aligned}$$

$$\begin{aligned} \frac{\partial y_F}{\partial t} + \frac{\partial Q_F}{\partial t} &= \left[D \nabla^2 y_F - (u \cdot \nabla) y_F - A (Q_F + y_F) y_0 - A (Q_0 + y_0) y_F \right] \\ &\quad + D (\nabla z \cdot \nabla z) \frac{\partial^2 Q_F}{\partial z^2} - A Q_F Q_0. \end{aligned}$$

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Define the conditional dissipation $N(\vec{x}, t) = D(\nabla z \cdot \nabla z)$.
and define the conditional average:

$$\tilde{N}(z) = \langle N | z \rangle.$$

and expand

$$N(\vec{x}, t) = \tilde{N}(z(\vec{x}, t)) + \eta(\vec{x}, t).$$

Then the CMC equation becomes:

~~$$\frac{\partial y_F}{\partial t} + \frac{\partial Q_F}{\partial t} = (N + \eta) \frac{\partial^2 Q_F}{\partial z^2} - A Q_F Q_0 + [D \nabla^2 y_F - (u \cdot \nabla) y_F - A(Q_F + y_F) y_0]$$~~

$$\frac{\partial y_F}{\partial t} + \frac{\partial Q_F}{\partial t} = (\tilde{N} + \eta) \frac{\partial^2 Q_F}{\partial z^2} - A Q_F Q_0 + [D \nabla^2 y_F - (u \cdot \nabla) y_F - 2A y_F y_0 - A(Q_F y_0 + Q_0 y_F)]$$

This is an equation true to every point of our volume.

If we take a conditional average across the volume on z then those quantities that are independent of $\vec{x} = (x, y, z)$ will remain invariant. So:

$$\left\langle \frac{\partial Q_F}{\partial t} | z \right\rangle = \frac{\partial Q_F}{\partial t}$$

$$\left\langle \tilde{N} \frac{\partial^2 Q_F}{\partial z^2} | z \right\rangle = \tilde{N} \frac{\partial^2 Q_F}{\partial z^2}$$

$$\langle A Q_F Q_0 | z \rangle = A Q_F Q_0$$

A few other quantities will vanish:

$$\left\langle \frac{\partial y_F}{\partial t} | z \right\rangle = \frac{\partial}{\partial t} \langle y_F | z \rangle = 0$$

$$\left\langle \eta \frac{\partial^2 Q_F}{\partial z^2} | z \right\rangle = \frac{\partial^2 Q_F}{\partial z^2} \langle \eta | z \rangle = 0$$

$$\langle A(Q_F y_0 + Q_0 y_F) | z \rangle = A Q_F \langle y_0 | z \rangle + A Q_0 \langle y_F | z \rangle = 0 + 0 = 0$$

and a few others will not vanish:

$$\langle \nabla^2 y_F | z \rangle, \langle (u \cdot \nabla) y_F | z \rangle, \langle y_F y_0 | z \rangle.$$

It follows that:

$$\frac{\partial Q_F}{\partial t} = \tilde{N} \frac{\partial^2 Q_F}{\partial z^2} - A Q_F Q_0 + \langle D \nabla^2 y_F - (u \cdot \nabla) y_F - 2A y_F y_0 | z \rangle$$

In a similar manner we obtain:

$$\frac{\partial Q_0}{\partial t} = \tilde{N} \frac{\partial^2 Q_0}{\partial z^2} - r A Q_F Q_0 + \langle D \nabla^2 y_0 - (u \cdot \nabla) y_0 - 2A y_F y_0 | z \rangle.$$

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A critical assumption here is that the conditional average terms are negligible. Then we obtain:

$$\begin{aligned} \frac{\partial Q_F}{\partial t} &= \tilde{N}(z) \frac{\partial^2 Q_F}{\partial z^2} - A Q_F Q_0 \\ \frac{\partial Q_0}{\partial t} &= \tilde{N}(z) \frac{\partial^2 Q_0}{\partial z^2} - r A Q_F Q_0 \end{aligned}$$

The critical assumption is that

$$\varepsilon_F(n, t) = \langle D \nabla^2 y_F - (u \cdot \nabla) y_F - 2A y_F y_0 | z = n \rangle_t$$

and

$$\varepsilon_0(n, t) = \langle D \nabla^2 y_0 - (u \cdot \nabla) y_0 - 2A r y_F y_0 | z = n \rangle_t$$

are negligible. This should be verified numerically.

Boundary conditions

These equations are valid for $0 \leq z \leq 1$, therefore we need boundary conditions for

$$Q_F(0, t) = \langle Y_F | z = 0 \rangle$$

$$Q_F(1, t) = \langle Y_F | z = 1 \rangle$$

and

$$Q_0(0, t) = \langle Y_F | z = 0 \rangle, \quad Q_0(1, t) = \langle Y_F | z = 1 \rangle$$

Recall that

$$z = \frac{r Y_F - Y_0 + 1}{r + 1}$$

and $0 \leq Y_F \leq 1$ and $0 \leq Y_0 \leq 1$

a) Suppose that $z = 0$. Then

$$\frac{r Y_F - Y_0 + 1}{r + 1} = 0 \Leftrightarrow Y_0 = r Y_F + 1.$$

$$Y_0 \leq 1 \Rightarrow r Y_F + 1 \leq 1 \Rightarrow Y_F \leq 0. \quad \} \Rightarrow Y_F = 0.$$

Moreover $Y_F \geq 0$

and $Y_0 = r \cdot 0 + 1 = 1$.

$$\text{Therefore } (z = 0 \Rightarrow Y_F = 0 \wedge Y_0 = 1) \Rightarrow \begin{cases} Q_F(0, t) = 0 \\ Q_0(0, t) = 1. \end{cases}$$

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b) Suppose that $z=0$. Then,

$$\frac{rY_F - Y_0 + 1}{r+1} = 1 \Leftrightarrow rY_F - Y_0 = r \Leftrightarrow \underline{Y_0 = r(Y_F - 1)}$$

$$Y_F \leq 1 \Rightarrow Y_0 = r(Y_F - 1) \leq 0 \quad \left. \vphantom{Y_F \leq 1} \right\} \Rightarrow Y_0 = 0.$$

but also $Y_0 \geq 0$

It follows that $r(Y_F - 1) = 0 \Leftrightarrow Y_F = 1$.

$$\text{Therefore } (z=1 \Rightarrow Y_F=1 \wedge Y_0=0) \Rightarrow \begin{cases} Q_F(0,t) = 1 \\ Q_B(1,t) = 0 \end{cases}$$

We obtain then the following boundary conditions:

$$\begin{array}{ll} Q_F(0,t) = 0 & \text{and } Q_B(0,t) = 1 \\ Q_F(1,t) = 1 & Q_B(1,t) = 0. \end{array}$$

Remark.

If we solve the equation

$$\frac{\partial z}{\partial t} + (u \cdot \nabla) z = D \nabla^2 z$$

for "counterflow" we obtain

$$\tilde{N}(z) = N_0 \exp \left\{ -2 \left[\text{erf}^{-1}(2z-1) \right]^2 \right\}$$

What does this mean?

Derivation of the product CMC equation.

The CMC equation for fuel + oxidizer is:

$$\frac{\partial Q_F}{\partial t} = \tilde{N}(z,t) \frac{\partial^2 Q_F}{\partial z^2} - A Q_F Q_0$$

$$\frac{\partial Q_0}{\partial t} = \tilde{N}(z,t) \frac{\partial^2 Q_0}{\partial z^2} - r A Q_F Q_0$$

where $Q_F(n,t) = \langle Y_F | z=n \rangle_t$ $\tilde{N}(z,t) = \langle N | z=n \rangle_t$
 $Q_0(n,t) = \langle Y_0 | z=n \rangle_t$

with boundary conditions

$$Q_F(0,t) = 0 \quad Q_0(0,t) = 1$$

$$Q_F(1,t) = 1 \quad Q_0(1,t) = 0$$

Fact 1: Q_F, Q_0 are related by $\frac{r Q_F - Q_0 + 1}{r+1} = z$.

Solve for $Q_0 = r Q_F - Q_0 + 1 - (r+1)z$

Fact 2: The conditional average of the product is

$$Q_P = 1 - Q_F - Q_0$$

We express Q_F, Q_0 in terms of Q_P :

$$Q_F + Q_0 = 1 - Q_P \Leftrightarrow Q_F + r Q_F + 1 - (r+1)z = 1 - Q_P \Leftrightarrow$$

$$\Leftrightarrow (r+1)Q_F + 1 - (r+1)z = 1 - Q_P \Leftrightarrow$$

$$\Leftrightarrow (r+1)Q_F = (r+1)z - Q_P \Leftrightarrow \boxed{Q_F = z - \frac{Q_P}{r+1}}$$

and

$$Q_0 = r Q_F + 1 - (r+1)z = r \left[z - \frac{Q_P}{r+1} \right] + 1 - (r+1)z =$$

$$= r z - \frac{r Q_P}{r+1} + 1 - r z - z =$$

$$= (1-z) - \frac{r Q_P}{r+1}$$

Putting these together:

$$\boxed{Q_F = z - \frac{Q_P}{r+1}}$$

$$\boxed{Q_0 = (1-z) - \frac{r Q_P}{r+1}}$$

To rewrite in terms of z_{st} use $\frac{1}{r+1} = z_{st}$ and $r = \frac{1-z_{st}}{z_{st}}$

$$\begin{cases} Q_F = z - z_{st} Q_P \\ Q_0 = (1-z) - (1-z_{st}) Q_P \end{cases}$$

Now note that

$$\frac{\partial Q_F}{\partial t} = -z_{st} \frac{\partial Q_P}{\partial t}$$

$$\text{and } \frac{\partial^2 Q_F}{\partial z^2} = \frac{\partial^2}{\partial z^2} [z - z_{st} Q_P] = -z_{st} \frac{\partial^2 Q_P}{\partial z^2}$$

We substitute to the CMC equation for the fuel:

$$\frac{\partial Q_F}{\partial t} - \tilde{N} \frac{\partial^2 Q_F}{\partial z^2} = \dot{w}_F \Leftrightarrow$$

$$\Leftrightarrow -z_{st} \left[\frac{\partial Q_P}{\partial t} - \tilde{N} \frac{\partial^2 Q_P}{\partial z^2} \right] = \dot{w}_F$$

$$\Leftrightarrow \frac{\partial Q_P}{\partial t} = \tilde{N} \frac{\partial^2 Q_P}{\partial z^2} - \frac{\dot{w}_F}{z_{st}}$$

where $\dot{w}_F = -A Q_F Q_0 = -A (z - z_{st} Q_P) [(1-z) - (1-z_{st}) Q_P]$

It follows that

$$\frac{\partial Q_P}{\partial t} = \tilde{N} \frac{\partial^2 Q_P}{\partial z^2} + \dot{w}_P$$

where $\dot{w}_P = + \frac{A}{z_{st}} (z - z_{st} Q_P) [(1-z) - (1-z_{st}) Q_P]$

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Numerical solution of the CMC equation

We want solver for problems of the form

$$\frac{\partial u}{\partial t} = b(x,t) \frac{\partial^2 u}{\partial x^2} + w(x,t,u), \quad x \in [a_0, a_1]$$

with Dirichlet boundary conditions.

Use a split scheme

diffusion term \rightarrow Crank-Nicolson scheme

inhomogeneity \rightarrow Runge-Kutta

Let $x_m = a_0 + (a_1 - a_0)m/M = a_0 + (a_1 - a_0)hm$

$$u_m^n = u(x_m, nk)$$

$$b_m^n = b(x_m, nk)$$

$$w_m^n = w(x_m, nk, u_m^n)$$

$$\text{where } h = 1/M$$

$$K = \text{timestep.}$$

Also define $\mu = K/h^2$

● Crank-Nicolson step

$$A_m^n u_{m-1}^{n+1} + B_m^n u_m^{n+1} + C_m^n u_{m+1}^{n+1} = D_m^n, \quad \forall m \in \{1, 2, \dots, M-1\}$$

where

$$A_m^n = -b_m^n \mu / 2, \quad \forall m \in \{2, \dots, M-1\}$$

$$B_m^n = 1 + b_m^n \mu, \quad \forall m \in \{1, \dots, M-1\}$$

$$C_m^n = -b_m^n \mu / 2, \quad \forall m \in \{1, \dots, M-2\}$$

~~Taking boundary conditions~~

$$D_m^n = u_m^n + \frac{1}{2} b_m^n \mu (u_{m-1}^n - 2u_m^n + u_{m+1}^n).$$

Taking boundary conditions into account:

$$\begin{bmatrix} B_1^n & C_1^n & 0 & 0 & 0 \\ A_2^n & B_2^n & C_2^n & 0 & 0 \\ 0 & A_m^n & B_m^n & C_m^n & 0 \\ 0 & 0 & A_{M-2}^n & B_{M-2}^n & C_{M-2}^n \\ 0 & 0 & 0 & A_{M-1}^n & B_{M-1}^n \end{bmatrix} \begin{bmatrix} u_1^{n+1} \\ u_2^{n+1} \\ u_m^{n+1} \\ u_{M-2}^{n+1} \\ u_{M-1}^{n+1} \end{bmatrix} = \begin{bmatrix} D_1^n - u_0^n A_1^n \\ D_2^n \\ D_m^n \\ D_{M-2}^n \\ D_{M-1}^n - u_M^n C_{M-1}^n \end{bmatrix}$$

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To solve the tridiagonal system with Thomas algorithm the matrix must be diagonally dominant.

$$|B_m^n| \geq |A_m^n| + |C_m^n| \Leftrightarrow |1 + b_m^n \mu| \geq |-b_m^n \mu/2| + |-b_m^n \mu/2| \Leftrightarrow$$

$$\Leftrightarrow |1 + b_m^n \mu| \geq |b_m^n \mu| \Leftrightarrow (1 + b_m^n \mu)^2 \geq (b_m^n \mu)^2 \Leftrightarrow 1 + 2b_m^n \mu \geq 0$$

$$\Leftrightarrow b_m^n \mu \geq -\frac{1}{2}.$$

The requirement will be true if $b(x, t) \geq 0$ as it is expected in a parabolic system.

● Runge-kutta step for the inhomogeneity

Define: $k_1 = kw(x_m, nk, u_m^n)$

$$k_2 = kw(x_m + h/2, nk, u_m^n + k_1/2)$$

$$k_3 = kw(x_m + h/2, nk, u_m^n + k_2/2)$$

$$k_4 = kw(x_m + h, nk, u_m^n + k_3).$$

and then:

$$u_m^{n+1} = u_m^n + \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4).$$

● Test cases

To test the reliability of the solver one can use the following test cases:

a) Simple diffusion:

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} \quad \text{with} \quad u(x,0) = \sin(2nx) \quad , \quad \forall x \in [0,1]$$

has solution $u(x,t) = \sin(2nx) e^{-4n^2 t}$

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} - u \quad \text{with} \quad u(x,0) = \sin(2nx) \quad , \quad \forall x \in [0,1]$$

has solution $u(x,t) = \sin(2nx) e^{-(4n^2+1)t}$

b) Diffusion with variable diffusion coefficient

$$i) \quad \frac{\partial u}{\partial t} = x(1-x) \frac{\partial^2 u}{\partial x^2} \quad \text{with} \quad u(x,0) = x(1-x)$$

has solution $u(x,t) = x(1-x) e^{-2t}$

$$\frac{\partial u}{\partial t} = x(1-x) \frac{\partial^2 u}{\partial x^2} + (2-\lambda)u \quad \text{with} \quad u(x,0) = x(1-x)$$

has solution $u(x,t) = x(1-x) e^{-\lambda t}$

$$\frac{\partial u}{\partial t} = x(1-x) \frac{\partial^2 u}{\partial x^2} + [x(1-x) + u]$$

has solution $u(x,t) = x(1-x)(1-e^{-t})$

c) The boundary value problem:

$$x(1-x) \frac{\partial^2 u}{\partial x^2} = x(1-x) + u$$

with $u(0) = u(1) = 0$

has solution $u(x) = x(1-x)$.

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▼ Counterflow problem

Suppose that $\vec{u} = (u, v, w)$ is given by

$$\text{and that } \begin{matrix} u = ax, & v = -ay, & w = 0 \\ \text{at } t = 0 \end{matrix}$$

$$z(x, y, t = 0) = \begin{cases} 0 & y > 0 \\ 1 & y < 0 \end{cases}$$

The evolution equation for z is:

$$\frac{\partial z}{\partial t} + (u \cdot \nabla)z - D \nabla^2 z = 0 \Leftrightarrow$$

$$\Leftrightarrow \frac{\partial z}{\partial t} + ax \frac{\partial z}{\partial x} - ay \frac{\partial z}{\partial y} - D \left(\frac{\partial^2 z}{\partial x^2} + \frac{\partial^2 z}{\partial y^2} \right) = 0$$

Suppose we ignore the x dependence. Then:

$$\boxed{\frac{\partial z}{\partial t} - ay \frac{\partial z}{\partial y} - D \frac{\partial^2 z}{\partial y^2} = 0.}$$

with boundary condition $z(y, 0) = \begin{cases} 0 & y > 0 \\ 1 & y < 0 \end{cases}$

and $z(+\infty, t) = 1, z(-\infty, t) = 0.$

$$N(y, t) = D(\nabla z \cdot \nabla z) = D \left(\frac{\partial z}{\partial y} \right)^2$$

To solve the PDE let

$$z(y, t) = c_1 + c_2 \operatorname{erf} \left(\frac{y}{\delta(t)} \right)$$

where $\operatorname{erf} x = \frac{2}{\sqrt{\pi}} \int_0^x e^{-t^2} dt \rightarrow$ error function.

$$\text{Note that } \frac{d}{dx} \operatorname{erf}(x) = \frac{2}{\sqrt{\pi}} \frac{d}{dx} \int_0^x e^{-t^2} dt = \frac{2e^{-x^2}}{\sqrt{\pi}}$$

It follows that

$$\begin{aligned} \frac{\partial z}{\partial t} &= c_2 \frac{\partial}{\partial t} \operatorname{erf} \left(\frac{y}{\delta(t)} \right) = c_2 \frac{2}{\sqrt{\pi}} \exp \left(-\frac{y^2}{\delta^2(t)} \right) \frac{\partial}{\partial t} \left(\frac{y}{\delta(t)} \right) = \\ &= \frac{2c_2}{\sqrt{\pi}} e^{-y^2/\delta^2} \frac{-y}{\delta^2(t)} \frac{d\delta}{dt} \end{aligned}$$

(2)

and

$$\frac{\partial z}{\partial y} = c_2 \frac{\partial}{\partial y} \operatorname{erf}\left(\frac{y}{\delta(t)}\right) = c_2 \frac{2}{\sqrt{\pi}} \exp\left(-\frac{y^2}{\delta^2(t)}\right) \frac{\partial}{\partial t} \left(\frac{y}{\delta(t)}\right) =$$

$$= \frac{2c_2}{\sqrt{\pi}} e^{-y^2/\delta^2} \frac{1}{\delta(t)}$$

$$\frac{\partial^2 z}{\partial y^2} = \frac{2c_2}{\delta(t)\sqrt{\pi}} e^{-y^2/\delta^2} \frac{-2y}{\delta^2(t)}$$

To summarize:

$$\frac{\partial z}{\partial t} = \left[\frac{2c_2}{\sqrt{\pi}} e^{-y^2/\delta^2} \right] \frac{-y}{\delta^2(t)} \frac{d\delta}{dt}$$

$$\frac{\partial z}{\partial y} = \left[\frac{2c_2}{\sqrt{\pi}} e^{-y^2/\delta^2} \right] \frac{1}{\delta(t)}$$

$$\frac{\partial^2 z}{\partial y^2} = \left[\frac{2c_2}{\sqrt{\pi}} e^{-y^2/\delta^2} \right] \frac{-2y}{\delta^3(t)}$$

Substituting to the PDE we obtain:

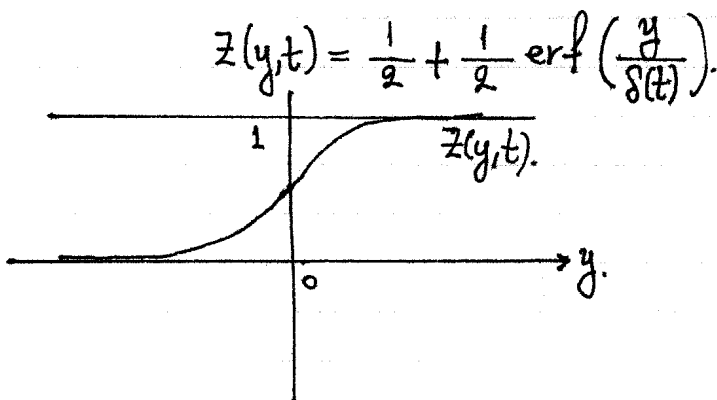
$$\frac{\partial z}{\partial t} - ay \frac{\partial z}{\partial y} - D \frac{\partial^2 z}{\partial y^2} = 0 \Leftrightarrow$$

$$-\frac{y}{\delta^2(t)} \frac{d\delta}{dt} - \frac{ay}{\delta(t)} + D \frac{2y}{\delta^3(t)} = 0 \Leftrightarrow$$

$$\bullet \frac{1}{\delta^2} \frac{d\delta}{dt} = \frac{2D}{\delta^3} - \frac{a}{\delta} \Leftrightarrow 2\delta \frac{d\delta}{dt} = 4D - 2a\delta^2 \Leftrightarrow$$

$$\Leftrightarrow \frac{d\delta^2}{dt} = 4D - 2a\delta^2$$

Note that this works even when a is time dependent.
For the case $z_{st} = 0.5$



Solving for y/δ : $2z = 1 + \operatorname{erf}(y/\delta) \Leftrightarrow \operatorname{erf}(y/\delta) = 1 - 2z \Leftrightarrow y/\delta = \operatorname{erf}^{-1}(1-2z)$

$$\Leftrightarrow y/\delta = \operatorname{inverf}(1-2z)$$

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Solving for y/δ : $2z = 1 + \operatorname{erf}(y/\delta) \Leftrightarrow \operatorname{erf}(y/\delta) = 2z - 1 \Leftrightarrow$
 $\Leftrightarrow y/\delta = \operatorname{inverf}(2z - 1)$

$$\begin{aligned} N(y,t) &= D(\nabla z \cdot \nabla z) = D\left(\frac{\partial z}{\partial y}\right)^2 = D\left[\frac{1}{2} \frac{\partial}{\partial y} \operatorname{erf}\left(\frac{y}{\delta(t)}\right)\right]^2 = \\ &= D\left[\frac{1}{2} \frac{2}{\sqrt{\pi}} \exp\left(-\frac{y^2}{\delta^2(t)}\right) \frac{1}{\delta(t)}\right]^2 = \\ &= D\left(\frac{1}{\delta(t)\sqrt{\pi}}\right)^2 \exp(-2y^2/\delta^2) = \\ &= N_0(t) \exp(-2 \operatorname{inverf}^2(2z-1)) = \tilde{N}(z,t) \Rightarrow \\ &\Rightarrow \boxed{\langle N|z \rangle_t = N_0(t) \exp[-2 \operatorname{inverf}^2(2z-1)]} \end{aligned}$$

What about $\delta(t)$ and $N_0(t)$?

Let's solve:

$$\frac{d\delta^2}{dt} = 4D - 2a(t)\delta^2 \Leftrightarrow \frac{d\delta^2}{dt} + 2a(t)\delta^2 = 4D.$$

Homogeneous solution:

$$\begin{aligned} \frac{d\delta_0^2}{dt} &= -2a(t)\delta_0^2 \Leftrightarrow \frac{1}{\delta_0^2} \frac{d\delta_0^2}{dt} = -2a(t) \Leftrightarrow \\ \Leftrightarrow \ln \delta_0^2 &= -2 \int a(t) dt \Leftrightarrow \delta_0^2 = \delta_0^2(0) \exp\left[-2 \int_0^t a(t) dt\right] \end{aligned}$$

Particular solution: $\delta_p(t) = 4Dt$ therefore:

$$\delta^2(t) = \delta_0^2 \exp\left[-2 \int_0^t a(t) dt\right] + 4Dt \Leftrightarrow \delta(t) \sim 2\sqrt{Dt}$$

and $N_0(t) \sim \frac{2}{t} \rightsquigarrow$ independent of D .

①

▼ Investigation of dependence of CMC on boundary conditions.

We want to investigate the behaviour of the product CMC equation and its dependence on $N(z,t)$ and boundary condition.

The equation:

$$\frac{\partial Q_p}{\partial t} = \tilde{N}(z,t) \frac{\partial^2 Q_p}{\partial z^2} + \frac{A}{z_{st}} (z - z_{st} Q_p) [(1-z) - (1-z_{st}) Q_p].$$

We can model $\tilde{N}(z,t)$ with counterflow:

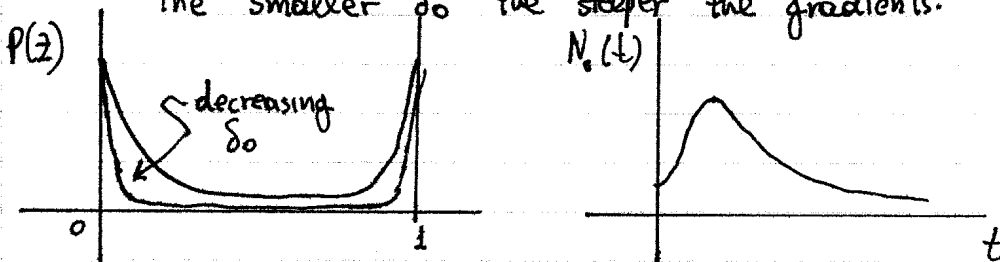
$$\tilde{N}(z,t) = \exp[-2 \operatorname{inverf}^2(2z-1)] N_0(t).$$

where $N_0(t) = \frac{D}{\pi(\delta_0 e^{-2at} + 4Dt)}$

The modeling parameters are δ_0 and a and their interpretation is the following:

δ_0 = the steepness of the $\frac{\partial z}{\partial t}$ gradient in the 1 regions to the 0 region in the initial condition.

The smaller δ_0 the steeper the gradients.



a = increases as the velocity field becomes more turbulent. i.e. increases as the Reynolds number increases.

For the counterflow problem the characteristic scales are:
 $u = al$, $l = \text{something}$ and $v = D$
 therefore the Reynolds number is:

$$Re = \frac{ul}{v} = \frac{al^2}{v}$$

● The meaning of a .

(2)

Note that a controls the peak of $N_0(t)$.

$$\frac{\partial N_0(t)}{\partial t} = \frac{D}{n} \frac{\partial}{\partial t} \left(\frac{1}{\delta_0 e^{-2at} + 4Dt} \right) = \frac{D}{n} \frac{-(4D - 2a\delta_0 e^{-2at})}{(\delta_0 e^{-2at} + 4Dt)^2} = 0$$

$$\Leftrightarrow 2a\delta_0 e^{-2at_0} = 4D \Leftrightarrow e^{-2at_0} = \frac{2D}{a\delta_0} \Leftrightarrow$$

$$\Leftrightarrow -2at_0 = \ln \frac{2D}{a\delta_0} \Leftrightarrow \boxed{t_0 = \frac{1}{2a} \ln \frac{a\delta_0}{2D}}$$

The peak value is:

$$4D = 2a\delta_0 e^{-2at} \Rightarrow N_{\max} = \frac{D}{n(\delta_0 e^{-2at} + 4Dt)} =$$

$$= \frac{D}{n\left(\frac{4D}{2a} + 4Dt_0\right)} = \frac{1}{n\left(\frac{2}{a} + 4Dt_0\right)} =$$

$$= \left[n\left(\frac{2}{a} + \frac{1}{2a} \ln \frac{a\delta_0}{2D}\right) \right]^{-1} = \frac{a}{n} \left(2 + \frac{1}{2} \ln \frac{a\delta_0}{2D} \right)^{-1}$$

$$= \frac{2a}{n\left(4 + \ln \frac{a\delta_0}{2D}\right)}$$

therefore:

$$\boxed{N_{\max} = \frac{2a}{n\left(4 + \ln \frac{a\delta_0}{2D}\right)}}$$

● The meaning of δ_0 .

The initial counterflow field is given by:

$$z(y, t) = \frac{1}{2} + \frac{1}{2} \operatorname{erf}\left(\frac{y}{\delta_0}\right)$$

The slopes are given by:

$$\frac{\partial z}{\partial y} = \frac{1}{2} \frac{\partial}{\partial y} \operatorname{erf}\left(\frac{y}{\delta_0}\right) = \frac{1}{4\sqrt{\pi}} \exp\left(-\frac{y^2}{\delta_0^2}\right) \frac{1}{\delta_0} \Rightarrow$$

$$\Rightarrow \left. \frac{\partial z}{\partial y} \right|_{y=0} = \frac{1}{4\sqrt{\pi} \delta_0} \quad \leadsto \text{at } y=0 \text{ we have maximum slope.}$$

so $\delta_0 \sim 1/\text{slope} \sim 1/k_{\max} \leadsto$

where $k_{\max} = \max$ integer wavenumber.

③

• The investigation.

Define $\tilde{N}(z, t; b) = \begin{cases} \tilde{N}(z, t) & \text{if } z \in [b, 1-b]. \\ 0 & \text{otherwise.} \end{cases}$

Time step CMC with $\tilde{N}(z, t) \rightarrow$ treat this as an exact solution

Time step CMC with $\tilde{N}(z, t; b) \rightarrow$ compare max-norm error as $e(t)$ and find point in time t where the error is largest.

b should control: maximum error e_{\max} .

time where the error is largest.

These should also depend in changes in a and δ_0 .

e_{\max} must also be checked against using $\langle Nt \rangle$.
as well as b -truncated $\langle N \rangle$.

\hookrightarrow effects on $Q_F(z, t)$, errors on $Q_F(z, t)$.
what about $\langle Y_F \rangle$?

Can $P(z, t, D)$ be known if it is known for $D=1$?

(1)

▼ Sensitivity of counterflow CMC on behaviour of $N(z,t)$

The CMC equation we study is:

$$\frac{\partial QP}{\partial t} = N(z,t) \frac{\partial^2 QP}{\partial z^2} + \frac{A}{zst} (z - zst QP) [(1-z) - (1-zst) QP]$$

The counterflow model of $N(z,t)$ is:

$$N(z,t) = N_0(t) \exp[-2 \text{inverf}^2(zz-1)]$$

where $N_0(t)$ must be obtained by simulation runs with the corresponding $P(z,t)$.

Then the average $N_0(t)$ can be obtained from

$$\langle N \rangle_t = \int_0^1 N(z,t) P(z,t) dz = N_0(t) \int_0^1 \exp[-2 \text{inverf}^2(zz-1)] P(z,t) dz$$

Let $\sigma^2 = \langle z^2 \rangle - \langle z \rangle^2$ be the variance of the z field.

It can be shown then that

$$\boxed{\frac{d\sigma^2}{dt} = -2 \langle N \rangle_t}$$

In order for $P(z,t)$ and $N_0(t)$ to make physical sense together, they must respect the relationship above.

Moreover, $P(z,t)$ can be modeled by:

$$P(z,t) = \frac{z^{a(t)-1} (1-z)^{b(t)-1}}{B(a,b)}$$

$$\text{where } a(t) = \mu \left[\frac{\mu(1-\mu)}{\sigma^2} - 1 \right] \quad \text{with } \begin{cases} \mu = \langle z \rangle \\ \sigma^2 = \langle z^2 \rangle - \langle z \rangle^2 \end{cases}$$

$$b(t) = \frac{a}{\mu} - a$$

Note of course that $\frac{d\mu}{dt} = 0$ so time dependence enters only by the variance.

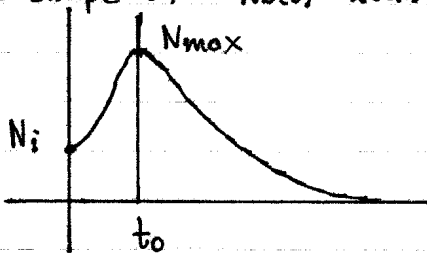
(9)

● Counterflow model for $N_0(t)$.

For the purposes of studying the CMC equation mathematically, we may use the expression for $N_0(t)$ obtained by the counterflow model:

$$N_0(t) = \frac{D}{n \delta^2(t)} \quad \text{where} \quad \delta^2(t) = \delta_0^2 e^{-2at} + 4Dt$$

The shape of $N_0(t)$ looks like this:



The characteristic values N_i , t_0 , N_{max} depend on D , δ_0 , a as follows:

a) N_i dependence

$$N_i = N_0(0) = \frac{D}{n \delta^2(0)} = \frac{D}{n [\delta_0^2 e^0 + 0]} = \frac{D}{n \delta_0^2} \rightarrow \text{not dependent on } a.$$

b) t_0 dependence

Note that

$$\frac{\partial N_0}{\partial t} = \frac{D}{n} \frac{\partial}{\partial t} \left(\frac{1}{\delta^2(t)} \right) = \frac{-D}{n \delta^4(t)} \frac{\partial \delta^2(t)}{\partial t} = 0 \Leftrightarrow$$

$$\Leftrightarrow \frac{\partial \delta^2}{\partial t} = \frac{\partial}{\partial t} [\delta_0^2 e^{-2at} + 4Dt] = -2a\delta_0^2 e^{-2at} + 4D = 0 \Leftrightarrow$$

$$\Leftrightarrow e^{-2at} = \frac{4D}{2a\delta_0^2} = \frac{2D}{a\delta_0^2} \Leftrightarrow -2at = \ln \frac{2D}{a\delta_0^2} \Leftrightarrow 2at = \ln \frac{a\delta_0^2}{2D}$$

$$\Leftrightarrow t = \frac{1}{2a} \ln \frac{a\delta_0^2}{2D}$$

Therefore we find that

$$t_0 = \frac{1}{2a} \ln \frac{a\delta_0^2}{2D}$$

(3)

c) At $t=t_0$, $4D = 2a\delta_0^2 e^{-2at}$ therefore:

$$N_{\max} = N(t_0) = \frac{D}{\pi \delta^2(t_0)} \quad \text{where:}$$

$$\delta^2(t_0) = \delta_0^2 e^{-2at_0} + 4Dt_0 = \frac{4D}{2a} + 4Dt_0 = 4D \left(\frac{1}{2a} + t_0 \right) =$$

$$= 4D \left[\frac{1}{2a} + \frac{1}{2a} \ln \frac{a\delta_0^2}{2D} \right] = \frac{2D}{a} \left[1 + \ln \frac{a\delta_0^2}{2D} \right] \Rightarrow$$

$$\Rightarrow N_{\max} = \frac{D}{\pi} \frac{a}{2D} \left(1 + \ln \frac{a\delta_0^2}{2D} \right)^{-1} = \frac{D}{2\pi} \left(1 + \ln \frac{a\delta_0^2}{2D} \right)^{-1}.$$

To summarize:

$$N_i = \frac{D}{\pi \delta_0^2}$$

$$t_0 = \frac{1}{2a} \ln \frac{a\delta_0^2}{2D}$$

$$N_{\max} = \frac{D}{2\pi} \left(1 + \ln \frac{a\delta_0^2}{2D} \right)^{-1}$$

● Sensitivity of the CMC equation.

Let $Q_p(z, t)$ be the solution using the counterflow based $N(z, t)$.
Let $b_1, b_2 \in [0, 1]$ with $b_1 < b_2$ and let:

$$N_1(z, t; b_1, b_2) = \begin{cases} N(z, t) & \text{if } b_1 \leq z \leq b_2 \\ 0 & \text{otherwise} \end{cases} \quad (\text{Stevé's way})$$

$$N_2(z, t; b_1, b_2) = \begin{cases} N(z, t) & , \text{ if } b_1 \leq z \leq b_2 \\ N(b_1, t) & , \text{ if } z < b_1 \\ N(b_2, t) & , \text{ if } b_2 < z \end{cases} \quad (\text{another way})$$

$$N_3(z, t; b_1, b_2) = \begin{cases} N(z, t) & , \text{ if } b_1 \leq z \leq b_2 \\ N(b_1, t) z / b_1 & , \text{ if } z < b_1 \\ N(b_2, t) (1-z) / (1-b_2) & , \text{ if } b_2 < z \end{cases} \quad (\text{Veljoni's way})$$

Solve the CMC equation with these and obtain the following solutions:

$$N_1(z, t; b_1, b_2) \longrightarrow Q_1(z, t; b_1, b_2)$$

$$N_2(z, t; b_1, b_2) \longrightarrow Q_2(z, t; b_1, b_2)$$

$$N_3(z, t; b_1, b_2) \longrightarrow Q_3(z, t; b_1, b_2)$$

and look at how much they deviate from $Q_p(z, t)$ in terms of the max-norm.